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Steady-state solutions for modified Stokes' second problem of Maxwell fluids with power-law dependence of viscosity on the pressure

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Abstract: Analytical expressions for the steady-state solutions of modified Stokes' second problem of a class of incompressible Maxwell fluids with power-law dependence of viscosity on the pressure are determined when the gravity effects are considered. Fluid motion is generated by a flat plate that oscillates in its plane. We discuss similar solutions for the simple Couette flow of the same fluids. Obtained results can be used by the experimentalists who want to know the required time to reach the steady or permanent state. Furthermore, we discuss the accuracy of results by graphical comparisons between the solutions corresponding to the motion due to cosine oscillations of the plate and simple Couette flow. Similar solutions for incompressible Newtonian fluids with power-law dependence of viscosity on the pressure performing the same motions and some known solutions from the literature are obtained as limiting cases of the present results. The influence of pertinent parameters on fluid motion is graphically underlined and discussed.

Keywords: Modified Stokes' second problem; Maxwell fluids; Pressure-dependent viscosity.

MSC: 76A05; 35B35; 35D35; 35B40.

1. Introduction

The motion of fluid over an infinite plate oscillating in its plane is termed as Stokes' second problem by Schlichting [1]. It is termed as the modified Stokes' second problem by Rajagopal *et al.*, [2] if the fluid is bounded by two parallel walls. Both motions are important from the theoretical and practical point of view because they appear in many applied problems, such as flows in vibrating media. If the fluid has been at rest up to the initial moment, its motion becomes steady in time and a very important problem for experimentalists is to know the time after which the steady or permanent state is obtained. To determine this time, at least the steady-state (permanent or long-time) solutions have to be known.

The fact that the fluid viscosity could depend on the pressure was early enough suggested by Stokes [3] and the experimental investigations (see for instance Bridgman [4], Cutler *et al.*, [5], Johnson and Tenaarwerk [6], Bair and Winer [7] and Prusa *et al.*, [8] have certified this supposition. For instance, in elastohydrodynamic lubrication problems, the effects of pressure on viscosity cannot be neglected. Concerning the importance of the pressure-dependent viscosity in steady motions of incompressible fluids, we recommend the paper of Huilgol, and You [9]. On the other hand, Kannan and Rajagopal [10] remarked that gravity has a notable influence in different motions with engineering applications. Its effects are more pronounced if the pressure alters along the direction in which the gravity acts. First exact solutions for steady motions of incompressible Newtonian fluids with pressure-dependent viscosity in which the influence of gravity is taken into consideration are those of Rajagopal [11,12]. Interesting steady and starting solutions for the modified Stokes' problems of Newtonian fluids with pressure-dependent viscosity have also been established by Prusa [13], respectively Rajagopal *et al.*, [12] when the gravity effects are taken into consideration. Recently, permanent solutions corresponding to motions of incompressible Newtonian fluids with power-law dependence of viscosity on the pressure have been determined by Fetecau, and Agop [14], Fetecau and Vieru [15], and Fetecau and Rauf [16]. Some of them have already been extended to incompressible Maxwell fluids (IMF) of the same type [17–19].

The goal of this work is to provide closed-form expressions for the steady-state solutions corresponding to the modified Stokes' second problem and the simple Couette flow for a class of IMF with power-law dependence of viscosity on the pressure. Analytical expressions are established for the dimensionless velocity fields and the corresponding nontrivial shear and normal stresses. For a check of their correctness, it was graphically proved that the diagrams of the solutions corresponding to the motion induced by cosine oscillations of the plate are almost identical to those of the simple Couette flow if the oscillations' frequency is small enough. In addition, similar solutions for ordinary IMF and incompressible Newtonian fluids (IMF) with power-law dependence of viscosity on the pressure performing the same motions are obtained as limiting cases of general results. The influence of the main parameters on the fluid motion is graphically underlined and discussed.

2. Formulation of the problem

Let us consider an IMF with pressure-dependent viscosity at rest between two infinite horizontal parallel plates at the distance d one of the other as it is illustrated in Figure 1. Its constitutive equations, as they have been presented by Karra *et al.*, [20], are given by the following relations

$$\mathbf{T} = -p\mathbf{I} + \mathbf{S}, \quad \mathbf{S} + \lambda \left(\frac{d\mathbf{S}}{dt} - \mathbf{L}\mathbf{S} - \mathbf{S}\mathbf{L}^T \right) = \eta(p)(\mathbf{L} + \mathbf{L}^T). \quad (1)$$

Here \mathbf{T} is the stress tensor, \mathbf{S} the extra-stress tensor, \mathbf{I} the unit tensor, \mathbf{L} is the gradient of the velocity vector \mathbf{v} and λ is the relaxation time of the fluid. The viscosity function $\eta(\cdot)$ to be here used has the following power-law form

$$\eta(p) = \mu [1 + \alpha(p - p_0)]^{4/3}, \quad (2)$$

where α is the pressure-viscosity coefficient and μ is the fluid viscosity at the reference pressure p_0 . We shall refer to the Lagrange multiplier p as pressure although, for such fluids, it is not the mean normal stress [20].

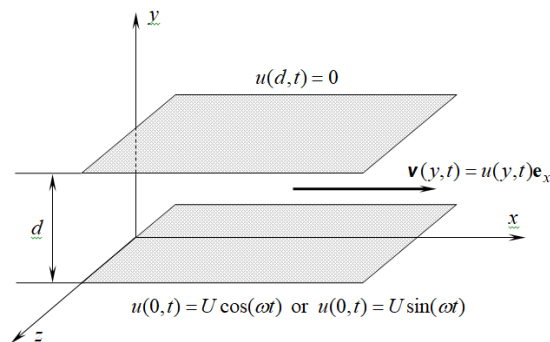


Figure 1. Geometry of the flow.

If $\lambda \rightarrow 0$ in the equality (1)₂, the new constitutive equations (1) define incompressible Newtonian fluids (INF) with pressure-dependent viscosity. If $\alpha = 0$ in Eq. (2) $\eta(p) = \mu$ and the adequate constitutive equations (1) correspond to ordinary IMF. The fact that $\eta(p) \rightarrow \infty$ for $p \rightarrow \infty$ is in accordance with a property that have been experimentally confirmed.

At the moment $t = 0^+$ the lower plate begins to oscillate in its plane according to

$$\mathbf{v} = U \cos(\omega t)\mathbf{e}_x \quad \text{or} \quad \mathbf{v} = U \sin(\omega t)\mathbf{e}_x, \quad (3)$$

where \mathbf{e}_x is the unit vector along the x -axis of a suitable Cartesian coordinate system x, y , and z whose y -axis is perpendicular to the plates while U and ω are the amplitude, respectively the frequency of the oscillations. Due to the shear the fluid begins to move and, as well as Karra *et al.*, [20], we are looking for a velocity field and pressure of the form

$$\mathbf{v} = \mathbf{v}(y, t) = u(y, t)\mathbf{e}_x, \quad p = p(y). \quad (4)$$

Assuming that the extra-stress tensor \mathbf{S} , as well as the fluid velocity \mathbf{v} is also a function of y and t only and using the fact that the fluid was at rest up to the moment $t = 0$, it is not difficult to show that the components

S_{xz} , S_{yy} , S_{yz} and S_{zz} of the extra-stress tensor S are zero while the non-trivial shear and normal stresses $\tau(y, t) = S_{xy}(y, t)$, respectively $\sigma(y, t) = S_{xx}(y, t)$ have to satisfy the following linear differential equations

$$\lambda \frac{\partial \tau(y, t)}{\partial t} + \tau(y, t) = \eta(p) \frac{\partial u(y, t)}{\partial y}, \quad \lambda \frac{\partial \sigma(y, t)}{\partial t} + \sigma(y, t) = 2\lambda \tau(y, t) \frac{\partial u(y, t)}{\partial y}. \quad (5)$$

In the absence of a pressure gradient in the flow direction, the balance of momentum reduces to the next two relevant partial or ordinary differential equations

$$\rho \frac{\partial u(y, t)}{\partial t} = \frac{\partial \tau(y, t)}{\partial y}, \quad \frac{dp(y)}{dy} = -\rho g, \quad (6)$$

while the incompressibility condition is identically satisfied. Into above relations ρ is the density of the fluid and g is the gravitational acceleration. Integrating the second equation with respect to y between the limits 0 and d , it results that

$$p(y) = \rho g(d - y) + p_0 \text{ where } p_0 = p(d). \quad (7)$$

Now, eliminating the shear stress $\tau(y, t)$ between the equalities (5)₁ and (6)₁ and bearing in mind the expressions of $\eta(p)$ and p from the equalities (2), respectively (7) one obtains for the dimensional velocity field $u(y, t)$ the following initial and boundary value problem

$$\mu [1 + \alpha \rho g(d - y)]^{4/3} \frac{\partial^2 u(y, t)}{\partial y^2} - \frac{4}{3} \mu \alpha \rho g [1 + \alpha \rho g(d - y)]^{1/3} \frac{\partial u(y, t)}{\partial y} = \rho \left(1 + \lambda \frac{\partial}{\partial t} \right) \frac{\partial u(y, t)}{\partial t}; \quad 0 < y < d, t > 0, \quad (8)$$

$$u(y, 0) = 0, \quad \left. \frac{\partial u(y, t)}{\partial t} \right|_{t=0} = 0; \quad 0 \leq y \leq d, \quad (9)$$

$$u(y, 0) = U \cos(\omega t) \text{ or } u(y, 0) = U \sin(\omega t), \quad u(d, t) = 0; \quad t > 0. \quad (10)$$

As soon as the fluid velocity $u(y, t)$ is known, the corresponding shear and normal stresses $\tau(y, t)$ and $\sigma(y, t)$ can be determined from the next linear differential equations

$$\lambda \frac{\partial \tau(y, t)}{\partial t} + \tau(y, t) = \mu [1 + \alpha \rho g(d - y)]^{4/3} \frac{\partial u(y, t)}{\partial y}; \quad 0 < y < d, t > 0, \quad (11)$$

$$\lambda \frac{\partial \sigma(y, t)}{\partial t} + \sigma(y, t) = 2\lambda \tau(y, t) \frac{\partial u(y, t)}{\partial y}; \quad 0 < y < d, t > 0. \quad (12)$$

Introducing the following non-dimensional variables, functions and parameters

$$y^* = \frac{y}{d}, \quad t^* = \frac{U}{d} t, \quad u^* = \frac{u}{U}, \quad \tau^* = \frac{1}{\rho U^2} \tau, \quad \sigma^* = \frac{1}{\rho U^2} \sigma, \quad \omega^* = \frac{d}{U} \omega, \quad \alpha^* = \alpha \rho g d, \quad (13)$$

in the governing equations (8)-(12) and dropping out the star notation, one obtains the next dimensionless initial and boundary value problem

$$[1 + \alpha(1 - y)]^{4/3} \frac{\partial^2 u(y, t)}{\partial y^2} - \frac{4}{3} \alpha [1 + \alpha(1 - y)]^{1/3} \frac{\partial u(y, t)}{\partial y} = \text{Re} \left(1 + \text{We} \frac{\partial}{\partial t} \right) \frac{\partial u(y, t)}{\partial t}; \quad 0 < y < 1, t > 0, \quad (14)$$

$$u(y, 0) = 0, \quad \left. \frac{\partial u(y, t)}{\partial t} \right|_{t=0} = 0; \quad 0 \leq y \leq 1, \quad (15)$$

$$u(0, t) = \cos(\omega t) \text{ or } u(0, t) = \sin(\omega t), \quad u(1, t) = 0; \quad t > 0, \quad (16)$$

for the velocity field $u(y, t)$ and the linear differential equations with initial conditions

$$\text{Re} \left(1 + \text{We} \frac{\partial}{\partial t} \right) \tau(y, t) = [1 + \alpha(1 - y)]^{4/3} \frac{\partial u(y, t)}{\partial y}, \quad \tau(y, 0) = 0; \quad 0 < y < 1, t > 0, \quad (17)$$

$$\left(1 + \text{We} \frac{\partial}{\partial t} \right) \sigma(y, t) = 2\text{We} \tau(y, t) \frac{\partial u(y, t)}{\partial y}, \quad \sigma(y, 0) = 0; \quad 0 < y < 1, t > 0, \quad (18)$$

for the shear and normal stresses. Into above relations $\text{Re} = Ud/\nu$ and $\text{We} = \lambda U/d$ are Reynolds, respectively Weissenberg dimensionless numbers and $\nu = \mu/\rho$ is the kinematic viscosity of the fluid.

3. Solution of the problem

In order to evade possible confusions, we denote by $u_c(y, t)$, $\tau_c(y, t)$, $\sigma_c(y, t)$ and $u_s(y, t)$, $\tau_s(y, t)$, $\sigma_s(y, t)$ the dimensionless starting solutions corresponding to the two motions induced by cosine, respectively sine oscillations of the lower plate. These solutions can be represented as sums of their permanent and transient components, namely

$$\begin{aligned} u_c(y, t) &= u_{cp}(y, t) + u_{ct}(y, t), & \tau_c(y, t) &= \tau_{cp}(y, t) + \tau_{ct}(y, t), \\ \sigma_c(y, t) &= \sigma_{cp}(y, t) + \sigma_{ct}(y, t); & 0 < y < 1, & \quad t > 0, \end{aligned} \tag{19}$$

$$\begin{aligned} u_s(y, t) &= u_{sp}(y, t) + u_{st}(y, t), & \tau_s(y, t) &= \tau_{sp}(y, t) + \tau_{st}(y, t), \\ \sigma_s(y, t) &= \sigma_{sp}(y, t) + \sigma_{st}(y, t); & 0 < y < 1, & \quad t > 0. \end{aligned} \tag{20}$$

Up to the moment $t = t_{cp}$ or $t = t_{sp}$ which is the time to reach the permanent state, the fluid behavior is described by the starting solutions. After this time, when the absolute values of the transient components are small enough and can be neglected, the fluid moves according to the permanent solutions $u_{cp}(y, t)$, $\tau_{cp}(y, t)$, $\sigma_{cp}(y, t)$, respectively $u_{sp}(y, t)$, $\tau_{sp}(y, t)$, $\sigma_{sp}(y, t)$ which are independent of the initial conditions but satisfy the boundary conditions and governing equations. In order to determine this time, which in practice is important for experimentalists, it is sufficient to know analytical expressions for the permanent solutions. To find these solutions in the same time for both motions, we define the non-dimensional complex velocity, shear stress and normal stress by the next relations

$$u_p(y, t) = u_{cp}(y, t) + iu_{sp}(y, t), \quad \tau_p(y, t) = \tau_{cp}(y, t) + i\tau_{sp}(y, t), \quad \sigma_p(y, t) = \sigma_{cp}(y, t) + i\sigma_{sp}(y, t), \tag{21}$$

where i is the imaginary unit.

The complex velocity $u_p(y, t)$ has to satisfy the following boundary value problem

$$[1 + \alpha(1 - y)]^{4/3} \frac{\partial^2 u_p(y, t)}{\partial y^2} - \frac{4}{3}\alpha [1 + \alpha(1 - y)]^{1/3} \frac{\partial u_p(y, t)}{\partial y} = \text{Re} \left(1 + \text{We} \frac{\partial}{\partial t} \right) \frac{\partial u_p(y, t)}{\partial t}; \quad 0 < y < 1, \quad t \in R, \tag{22}$$

$$u_p(0, t) = e^{i\omega t}, \quad u_p(1, t) = 0; \quad t \in R, \tag{23}$$

while the complex stresses $\tau_p(y, t)$ and $\sigma_p(y, t)$ have to be solutions of the ordinary linear differential equations

$$\text{Re} \left(1 + \text{We} \frac{\partial}{\partial t} \right) \tau_p(y, t) = [1 + \alpha(1 - y)]^{4/3} \frac{\partial u_p(y, t)}{\partial y}; \quad 0 < y < 1, \quad t \in R, \tag{24}$$

$$\left(1 + \text{We} \frac{\partial}{\partial t} \right) \sigma_p(y, t) = 2\text{We}\tau_p(y, t) \frac{\partial u_p(y, t)}{\partial y}; \quad 0 < y < 1, \quad t \in R. \tag{25}$$

Bearing in mind the form of the boundary conditions (23) and the linearity of the governing equations (22) and (24), we are looking for solutions of the form

$$u_p(y, t) = V(y)e^{i\omega t}, \quad \tau_p(y, t) = T(y)e^{i\omega t}, \quad \sigma_p(y, t) = S(y)e^{2i\omega t}, \tag{26}$$

where $V(y)$, $T(y)$ and $S(y)$ are complex functions.

3.1. Calculation of the complex velocity $u_p(y, t)$

By substituting $u_p(y, t)$ from Eq. (26)₁ in (22) and (23), one obtains for the function $V(y)$ the following ordinary differential equation with boundary conditions

$$[1 + \alpha(1 - y)]^{4/3} \frac{d^2 V(y)}{dy^2} - \frac{4}{3}\alpha [1 + \alpha(1 - y)]^{1/3} \frac{dV(y)}{dy} + \gamma^2 V(y) = 0; \quad 0 < y < 1, \quad V(0) = 1, \quad V(1) = 0, \tag{27}$$

where $\gamma = \sqrt{-i\omega \text{Re}(1 + i\omega \text{We})}$. Now, making the next changes of the independent spatial variable y and the unknown function $V(y)$

$$y = \frac{1 + \alpha - z^3}{\alpha}, \quad V(y) = \frac{1}{\sqrt{z}}W(z), \quad (28)$$

one obtains for the function $W(z)$ the following suitable ordinary differential equation

$$\frac{d^2W(z)}{dz^2} + \frac{1}{z} \frac{dW(z)}{dz} - \left(\frac{1}{4z^2} - \frac{9}{\alpha^2} \gamma^2 \right) W(z) = 0, \quad (29)$$

with the next boundary conditions

$$W(1) = 0, \quad W\left(\sqrt[3]{1+\alpha}\right) = \sqrt[6]{1+\alpha}. \quad (30)$$

Making a new change of independent variable, namely $z = \alpha r / (3\gamma)$, one attains to an Euler-Bessel equation whose well known general solution allow us to determine

$$W(z) = \sqrt[6]{1+\alpha} \left[\frac{Y_{1/2}(a)J_{1/2}(az) - J_{1/2}(a)Y_{1/2}(az)}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \right], \quad (31)$$

where $a = 3\gamma/\alpha$, $b = a \sqrt[3]{1+\alpha}$ while $J_{1/2}(\cdot)$ and $Y_{1/2}(\cdot)$ are Bessel standard functions of the order 1/2. By substituting $W(z)$ in (28)₂ and the obtained result in (26)₁, it results that

$$u_p(y, t) = \frac{\sqrt[6]{1+\alpha}}{\sqrt[6]{1+\alpha(1-y)}} \left[\frac{Y_{1/2}(a)J_{1/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{1/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \right] e^{i\omega t}. \quad (32)$$

Consequently, the permanent velocities $u_{cp}(y, t)$ and $u_{sp}(y, t)$ are given by the relations

$$u_{cp}(y, t) = \frac{\sqrt[6]{1+\alpha}}{\sqrt[6]{1+\alpha(1-y)}} \Re \left\{ \frac{Y_{1/2}(a)J_{1/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{1/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} e^{i\omega t} \right\}, \quad (33)$$

$$u_{sp}(y, t) = \frac{\sqrt[6]{1+\alpha}}{\sqrt[6]{1+\alpha(1-y)}} \Im \left\{ \frac{Y_{1/2}(a)J_{1/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{1/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} e^{i\omega t} \right\}, \quad (34)$$

where \Re and \Im denotes the real, respectively the imaginary part of that which follows. Of course, the boundary conditions (16) are clearly satisfied.

3.2. Calculation of the complex stresses $\tau_p(y, t)$ and $\sigma_p(y, t)$

By derivation of the equality (32) with respect to y one obtains

$$\frac{\partial u_p(y, t)}{\partial y} = \frac{\gamma \sqrt[6]{1+\alpha}}{\sqrt[6]{[1+\alpha(1-y)]^5}} \frac{Y_{1/2}(a)J_{3/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{3/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} e^{i\omega t}. \quad (35)$$

Substituting the expression of $\partial u_p(y, t) / \partial y$ in Eq. (24) and bearing in mind the relation (26)₂, it results for the complex shear stress $\tau_p(y, t)$ the expression

$$\tau_p(y, t) = \frac{\sqrt[6]{1+\alpha} \sqrt{1+\alpha(1-y)}}{\text{Re}} \frac{Y_{1/2}(a)J_{3/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{3/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \frac{\sqrt{-i\omega \text{Re}}}{\sqrt{1+i\omega \text{We}}} e^{i\omega t}. \quad (36)$$

Consequently, the permanent shear stresses $\tau_{cp}(y, t)$ and $\tau_{sp}(y, t)$ have the forms

$$\tau_{cp}(y, t) = \frac{\sqrt[6]{1+\alpha} \sqrt{1+\alpha(1-y)}}{\text{Re}} \Re \left\{ \frac{Y_{1/2}(a)J_{3/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{3/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \frac{\sqrt{-i\omega \text{Re}}}{\sqrt{1+i\omega \text{We}}} e^{i\omega t} \right\}, \quad (37)$$

$$\tau_{sp}(y, t) = \frac{\sqrt[6]{1+\alpha} \sqrt{1+\alpha(1-y)}}{\text{Re}} \Im \left\{ \frac{Y_{1/2}(a)J_{3/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{3/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \frac{\sqrt{-i\omega \text{Re}}}{\sqrt{1+i\omega \text{We}}} e^{i\omega t} \right\}. \quad (38)$$

Direct computations show that the complex normal stress $\sigma_p(y, t)$ has the form

$$\sigma_p(y, t) = -2\omega We \frac{\sqrt[3]{1+\alpha}}{\sqrt[3]{1+\alpha(1-y)}} \left[\frac{Y_{1/2}(a)J_{3/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{3/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \right]^2 \frac{ie^{2i\omega t}}{1+2i\omega We} \tag{39}$$

and the permanent solutions $\sigma_{cp}(y, t)$ and $\sigma_{sp}(y, t)$ can be immediately written as being

$$\sigma_{cp}(y, t) = -2\omega We \frac{\sqrt[3]{1+\alpha}}{\sqrt[3]{1+\alpha(1-y)}} \Re \left\{ \left[\frac{Y_{1/2}(a)J_{3/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{3/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \right]^2 \frac{ie^{2i\omega t}}{1+2i\omega We} \right\}, \tag{40}$$

$$\sigma_{sp}(y, t) = -2\omega We \frac{\sqrt[3]{1+\alpha}}{\sqrt[3]{1+\alpha(1-y)}} \Im \left\{ \left[\frac{Y_{1/2}(a)J_{3/2}(a \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(a)Y_{3/2}(a \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(a)J_{1/2}(b) - J_{1/2}(a)Y_{1/2}(b)} \right]^2 \frac{ie^{2i\omega t}}{1+2i\omega We} \right\}. \tag{41}$$

Finally, it is worth pointing out the fact that the similar dimensionless solutions

$$u_{Ncp}(y, t) = \frac{\sqrt[6]{1+\alpha}}{\sqrt[6]{1+\alpha(1-y)}} \Re \left\{ \frac{Y_{1/2}(c)J_{1/2}(c \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(c)Y_{1/2}(c \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(c)J_{1/2}(d) - J_{1/2}(c)Y_{1/2}(d)} e^{i\omega t} \right\}, \tag{42}$$

$$u_{Nsp}(y, t) = \frac{\sqrt[6]{1+\alpha}}{\sqrt[6]{1+\alpha(1-y)}} \Im \left\{ \frac{Y_{1/2}(c)J_{1/2}(c \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(c)Y_{1/2}(c \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(c)J_{1/2}(d) - J_{1/2}(c)Y_{1/2}(d)} e^{i\omega t} \right\}, \tag{43}$$

$$\tau_{Ncp}(y, t) = \frac{\sqrt[6]{1+\alpha}\sqrt{1+\alpha(1-y)}}{\Re} \Re \left\{ \frac{Y_{1/2}(c)J_{3/2}(c \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(c)Y_{3/2}(c \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(c)J_{1/2}(d) - J_{1/2}(c)Y_{1/2}(d)} \sqrt{-i\omega Re} e^{i\omega t} \right\}, \tag{44}$$

$$\tau_{Nsp}(y, t) = \frac{\sqrt[6]{1+\alpha}\sqrt{1+\alpha(1-y)}}{\Re} \Im \left\{ \frac{Y_{1/2}(c)J_{3/2}(c \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(c)Y_{3/2}(c \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(c)J_{1/2}(d) - J_{1/2}(c)Y_{1/2}(d)} \sqrt{-i\omega Re} e^{i\omega t} \right\}, \tag{45}$$

$$\sigma_{Ncp}(y, t) = -2\omega We \frac{\sqrt[3]{1+\alpha}}{\sqrt[3]{1+\alpha(1-y)}} \Re \left\{ \left[\frac{Y_{1/2}(c)J_{3/2}(c \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(c)Y_{3/2}(c \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(c)J_{1/2}(d) - J_{1/2}(c)Y_{1/2}(d)} \right]^2 ie^{2i\omega t} \right\}, \tag{46}$$

$$\sigma_{Nsp}(y, t) = -2\omega We \frac{\sqrt[3]{1+\alpha}}{\sqrt[3]{1+\alpha(1-y)}} \Im \left\{ \left[\frac{Y_{1/2}(c)J_{3/2}(c \sqrt[3]{1+\alpha(1-y)}) - J_{1/2}(c)Y_{3/2}(c \sqrt[3]{1+\alpha(1-y)})}{Y_{1/2}(c)J_{1/2}(d) - J_{1/2}(c)Y_{1/2}(d)} \right]^2 ie^{2i\omega t} \right\}, \tag{47}$$

corresponding to INF with power-law dependence of viscosity on the pressure performing the same motions are immediately obtained taking $We = 0$ in Eqs. (33), (34), (37), (38) (40) and (41). Into above relations $c = 3\sqrt{-i\omega Re} / \alpha$ and $d = c \sqrt[3]{1 + \alpha}$.

4. Results' validation

In order to validate the correctness of results which have been here obtained, we shall compare their limits for $\alpha \rightarrow 0$ or $\omega \rightarrow 0$ with known results from the literature, respectively with the similar solutions corresponding to the simple Couette flow of the same fluids.

4.1. Case $\alpha \rightarrow 0$; Modified Stokes' second problem for ordinary IMF

Using convenient asymptotic approximations of the Bessel functions, namely

$$J_\nu(z) \approx \sqrt{\frac{2}{\pi z}} \cos \left[z - \frac{(2\nu + 1)\pi}{4} \right], \quad Y_\nu(z) \approx \sqrt{\frac{2}{\pi z}} \sin \left[z - \frac{(2\nu + 1)\pi}{4} \right] \quad \text{for } |z| \gg 1, \tag{48}$$

it is not difficult to show that for small enough values of the pressure-viscosity coefficient α permanent solutions $u_{cp}(y, t)$ and $u_{sp}(y, t)$ can be approximated by the following relations

$$u_{cp}(y, t) \approx \frac{\sqrt[3]{1+\alpha}}{\sqrt[3]{1+\alpha(1-y)}} \Re e \left\{ \frac{\sin\{a[1-\sqrt[3]{1+\alpha(1-y)}]\}}{\sin[a(1-\sqrt[3]{1+\alpha})]} e^{i\omega t} \right\}, \quad (49)$$

$$u_{sp}(y, t) \approx \frac{\sqrt[3]{1+\alpha}}{\sqrt[3]{1+\alpha(1-y)}} \Im m \left\{ \frac{\sin\{a[1-\sqrt[3]{1+\alpha(1-y)}]\}}{\sin[a(1-\sqrt[3]{1+\alpha})]} e^{i\omega t} \right\}. \quad (50)$$

Now, substituting the Maclaurin series expansions of $[1+\alpha(1-y)]^{1/3}$ and $(1+\alpha)^{1/3}$ in the previous relations and taking their limits for $\alpha \rightarrow 0$, one recovers the permanent solutions corresponding to ordinary IMF performing the same motions, namely

$$\begin{aligned} u_{Ocp}(y, t) &= \lim_{\alpha \rightarrow 0} u_{cp}(y, t) = \Re e \left\{ \frac{\sin[\gamma(1-y)]}{\sin \gamma} e^{i\omega t} \right\}, \\ u_{Osp}(y, t) &= \lim_{\alpha \rightarrow 0} u_{sp}(y, t) = \Im m \left\{ \frac{\sin[\gamma(1-y)]}{\sin \gamma} e^{i\omega t} \right\}. \end{aligned} \quad (51)$$

Indeed, using the known relations $\sin(iz) = i \sinh(z)$ and $\sqrt{-i} = -i\sqrt{i}$, it results that

$$u_{Ocp}(y, t) = \Re e \left\{ \frac{\sinh[\delta(1-y)]}{\sinh \delta} e^{i\omega t} \right\}, \quad u_{Osp}(y, t) = \Im m \left\{ \frac{\sinh[\delta(1-y)]}{\sinh \delta} e^{i\omega t} \right\}, \quad (52)$$

where $\delta = \sqrt{i\omega Re(1+i\omega We)}$. As expected, the expression of $u_{Osp}(y, t)$ from Eq. (52)₂ is identical to that obtained by Fetecau *et al.*, [21, Eq. (36) with $K = 0$].

Similar computations show that the stresses $\tau_{cp}(y, t)$, $\tau_{sp}(y, t)$, $\sigma_{cp}(y, t)$ and $\sigma_{sp}(y, t)$ can be approximated by the following relations:

$$\tau_{cp}(y, t) \approx \frac{-\sqrt[3]{1+\alpha} \sqrt[3]{1+\alpha(1-y)}}{Re} \Re e \left\{ \frac{\cos[\gamma(1-y)]}{\sin \gamma} \frac{\sqrt{-i\omega Re}}{\sqrt{1+i\omega We}} e^{i\omega t} \right\}, \quad (53)$$

$$\tau_{sp}(y, t) \approx \frac{-\sqrt[3]{1+\alpha} \sqrt[3]{1+\alpha(1-y)}}{Re} \Im m \left\{ \frac{\cos[\gamma(1-y)]}{\sin \gamma} \frac{\sqrt{-i\omega Re}}{\sqrt{1+i\omega We}} e^{i\omega t} \right\}. \quad (54)$$

$$\sigma_{cp}(y, t) \approx 2\omega We \frac{\sqrt{1+\alpha}}{\sqrt{1+\alpha(1-y)}} \Re e \left\{ \frac{\cos^2[\gamma(1-y)]}{\sin^2 \gamma} \frac{ie^{2i\omega t}}{1+2i\omega We} \right\}, \quad (55)$$

$$\sigma_{sp}(y, t) \approx 2\omega We \frac{\sqrt{1+\alpha}}{\sqrt{1+\alpha(1-y)}} \Im m \left\{ \frac{\cos^2[\gamma(1-y)]}{\sin^2 \gamma} \frac{ie^{2i\omega t}}{1+2i\omega We} \right\}. \quad (56)$$

Using again the previous identities and the fact that $\cos(iz) = \cosh(z)$ in the equalities (53), (54), (55) and (56) and taking their limits for $\alpha \rightarrow 0$, it results that

$$\tau_{Ocp}(y, t) = \lim_{\alpha \rightarrow 0} \tau_{cp}(y, t) = -\frac{1}{Re} \Re e \left\{ \frac{\cosh[\delta(1-y)]}{\sinh \delta} \frac{\sqrt{i\omega Re}}{\sqrt{1+i\omega We}} e^{i\omega t} \right\}, \quad (57)$$

$$\tau_{Osp}(y, t) = \lim_{\alpha \rightarrow 0} \tau_{sp}(y, t) = -\frac{1}{Re} \Im m \left\{ \frac{\cosh[\delta(1-y)]}{\sinh \delta} \frac{\sqrt{i\omega Re}}{\sqrt{1+i\omega We}} e^{i\omega t} \right\}, \quad (58)$$

$$\sigma_{Ocp}(y, t) = \lim_{\alpha \rightarrow 0} \sigma_{cp}(y, t) = 2\omega We \Re e \left\{ \frac{\cos^2 h^2[\delta(1-y)]}{\sin^2 h^2 \delta} \frac{ie^{2i\omega t}}{1+2i\omega We} \right\}, \quad (59)$$

$$\sigma_{Osp}(y, t) = \lim_{\alpha \rightarrow 0} \sigma_{sp}(y, t) = 2\omega We \Im m \left\{ \frac{\cos^2 h^2[\delta(1-y)]}{\sin^2 h^2 \delta} \frac{ie^{2i\omega t}}{1+2i\omega We} \right\}. \quad (60)$$

As it was to be expected, the expression of $\tau_{Osp}(y, t)$ from Eq. (58) is identical to that obtained by Fetecau *et al.*, [21, Eq. (42) with $K = 0$] by a different technique.

4.2. Case $\omega \rightarrow 0$; Simple Couette flow of IMF with power-law dependence of viscosity on the pressure

The dimensionless permanent solutions corresponding to the simple Couette flow of IMF with power-law dependence of the form (2) of velocity on the pressure, namely

$$\begin{aligned}
 u_{Cp}(y) &= \frac{\sqrt[3]{1+\alpha}}{1-\sqrt[3]{1+\alpha}} \left[\frac{1}{\sqrt[3]{1+\alpha(1-y)}} - 1 \right], \quad \tau_{Cp} = \frac{\alpha \sqrt[3]{1+\alpha}}{3Re(1-\sqrt[3]{1+\alpha})}, \\
 \sigma_{Cp}(y) &= \frac{2We}{9Re} \frac{\alpha^2 \sqrt[3]{(1+\alpha)^2}}{(1-\sqrt[3]{1+\alpha})^2} \frac{1}{\sqrt[3]{[1+\alpha(1-y)]^4}}; \quad 0 < y < 1, \quad t > 0,
 \end{aligned}
 \tag{61}$$

can be easily determined successively solving the corresponding governing equations. As expected, Figures 2-4 show that the diagrams of $u_{cp}(y, t)$, $\tau_{cp}(y, t)$ and $\sigma_{cp}(y, t)$ are almost identical to those of $u_{Cp}(y)$, τ_{Cp} , respectively $\sigma_{Cp}(y)$ if the frequency ω of the oscillations as well as the product ωt is small enough. A surprising result is the fact that the permanent shear stress τ_{Cp} corresponding to the simple Couette flow of such fluids is constant on the whole flow domain although the fluid velocity $u_{Cp}(y)$ and the corresponding normal stress $\sigma_{Cp}(y)$ are functions of the spatial variable y . However, this shear stress as well as the fluid velocity and the normal stress depend on the pressure-viscosity coefficient.

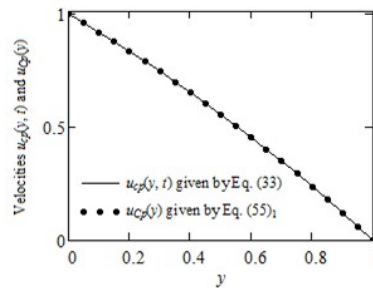


Figure 2. Comparison between the permanent the velocities $u_{cp}(y, t)$ and $u_{Cp}(y)$ for $Re = 100$, $We = 0.3$, $\alpha = 0.4$, $\omega = 0.001$ and $t = 10$

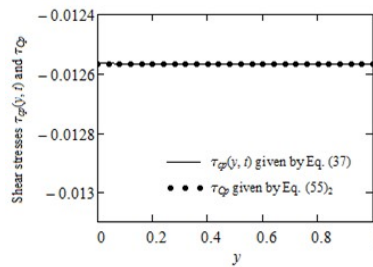


Figure 3. Comparison between the shear stresses $\tau_{cp}(y, t)$ and τ_{Cp} for $Re = 100$, $We = 0.3$, $\alpha = 0.4$, $\omega = 0.001$ and $t = 10$

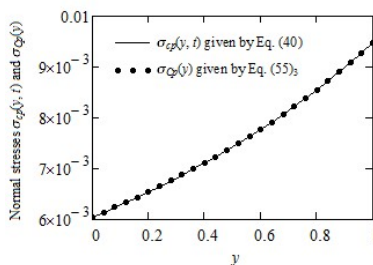


Figure 4. Comparison between the normal stresses $\sigma_{cp}(y, t)$ and $\sigma_{Cp}(y)$ for $Re = 100$, $We = 0.3$, $\alpha = 0.4$, $\omega = 0.001$ and $t = 10$

4.3. Case $\alpha \rightarrow 0$ and $\omega \rightarrow 0$ Simple Couette flow of ordinary IMF

Finally, making $\omega \rightarrow 0$ in Eqs. (52)₁, (57) and (59) or $\alpha \rightarrow 0$ in Eqs. (61) one obtains the steady solutions corresponding to the simple Couette flow of ordinary IMF, namely

$$u_{OCp}(y) = \lim_{\omega \rightarrow 0} u_{OCp}(y, t) = \lim_{\alpha \rightarrow 0} u_{Cp}(y) = 1 - y = u_{ONCp}(y), \tag{62}$$

$$\tau_{\text{OCp}} = \lim_{\omega \rightarrow 0} \tau_{\text{OCp}}(y, t) = \lim_{\alpha \rightarrow 0} \tau_{\text{Cp}} = -\frac{1}{\text{Re}} = \tau_{\text{ONCp}}, \quad (63)$$

$$\sigma_{\text{OCp}}(y) = \lim_{\omega \rightarrow 0} \sigma_{\text{OCp}}(y, t) = \lim_{\alpha \rightarrow 0} \sigma_{\text{Cp}}(y) = 2 \frac{\text{We}}{\text{Re}}. \quad (64)$$

The first two steady solutions $u_{\text{OCp}}(y)$ and τ_{OCp} are identical to the similar solutions $u_{\text{ONCp}}(y)$, respectively τ_{ONCp} corresponding to the simple Couette flow of ordinary INF and the expression of the velocity field given by Eq. (62) has been previously obtained by Erdogan [22]. In exchange, as it results from Eq. (64), the steady normal stress corresponding to the same motion of ordinary incompressible Newtonian fluids is zero.

5. Some numerical results and conclusions

The main purpose of this note is to offer a simple alternative for those who want to find the necessary time to reach the permanent state (steady state) corresponding to the modified Stokes' second problem of some IMF with power-law dependence of viscosity on the pressure. To do that, exact expressions are established for the dimensionless permanent solutions corresponding to the velocity field and the non-trivial shear and normal stresses. The required time to touch the permanent state can be graphically determined by comparing these solutions with the corresponding starting solutions (numerical solutions). It is the time after which the diagrams of starting solutions superpose over those of the permanent solutions and the fluid behavior is characterized by the steady-state solutions only.

For completion, as well as for a check of the correctness of results that have been here obtained; exact expressions are also determined for the similar solutions correspond to the simple Couette flow of the same fluids. Figures 2-4, as it was to be expected, clearly show that for a small enough value of the oscillations' frequency ω the diagrams of solutions $u_{\text{cp}}(y, t)$, $\tau_{\text{cp}}(y, t)$ and $\sigma_{\text{cp}}(y, t)$ are almost identical to those of the simple Couette flow $u_{\text{Cp}}(y)$, τ_{Cp} and $\sigma_{\text{Cp}}(y)$, respectively. The dimensionless steady state solutions corresponding to the ordinary IMF performing the same motions, as well as those of the INF with power-law dependence of viscosity on the pressure is obtained as limiting cases of the initial solutions.

In order to bring to light the influence of Weissenberg number We and of the pressure-viscosity coefficient α on the fluid motion Figures 5 and 6 and Table 1 have been included here. In these figures the time variations of the mid plane velocities $u_{\text{cp}}(0.5, t)$ and $u_{\text{sp}}(0.5, t)$ are presented at distinct values of the two parameters. Oscillatory specific features of the two motions and the phase difference between them are clearly visualized. It also results that the order of magnitude of the oscillations' amplitude for common values of the parameters is the same for both movements and the smaller values of pressure-viscosity coefficient α or We the smaller the oscillations' amplitude. Consequently, the fluid decelerates for decreasing values of the two parameters, and the lowest velocity corresponds to the ordinary IMF, respectively the INF with pressure-dependent viscosity. As regards the Weissenberg number We , as it was proved by Poole [23], it represents the ratio of elastic to viscous forces. Therefore, at the same elastic properties of the fluid, a decline of We means an increase of viscous forces, which implies a decrease of the fluid velocity. In Table 1, for completion, numerical values of the dimensionless steady velocity $u_{\text{Cp}}(y)$ corresponding to the simple Couette flow of IMF with power-law dependence of viscosity on the pressure are provided at three values of the pressure-viscosity coefficient α and different values of the spatial variable y . The fluid velocity, as before, grows for increasing values of α .

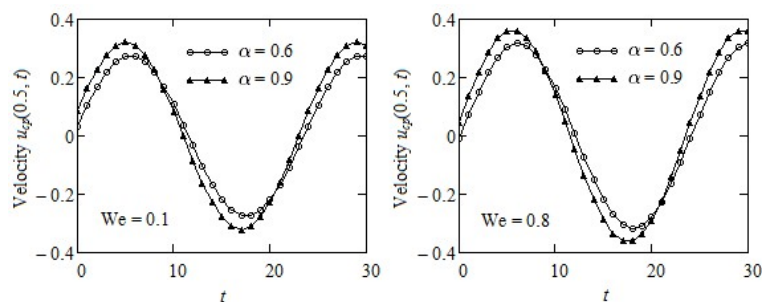


Figure 5. Profiles of velocities $u_{\text{cp}}(0.5, t)$ for $\text{Re} = 100$, $\omega = \pi/12$, $\alpha = 0.6$ and $\alpha = 0.9$ and two values of Weissenberg number We .

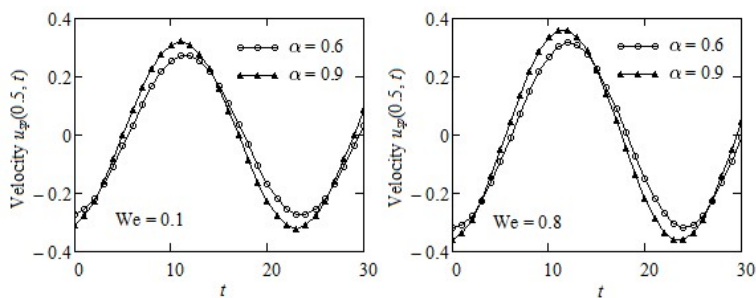


Figure 6. Profiles of velocities $u_{sp}(y, t)$ for $Re = 100$, $\omega = \pi/12$, $\alpha = 0.6$ and $\alpha = 0.9$ and two values of Weissenberg number We .

Table 1

y	Velocity $u_{Cp}(y)$		
	$\alpha = 0.2$	$\alpha = 0.5$	$\alpha = 0.9$
0	1	1	1
0.1	0.910	0.921	0.932
0.2	0.819	0.839	0.859
0.3	0.725	0.753	0.780
0.4	0.629	0.662	0.696
0.5	0.530	0.567	0.605
0.6	0.430	0.466	0.506
0.7	0.326	0.360	0.398
0.8	0.220	0.247	0.279
0.9	0.112	0.128	0.147
1	0	0	0

The main results that have been obtained by means of the present study are:

- Exact expressions have been established for the steady-state solutions of the modified Stokes’ second problem of IMF with power-law dependence of viscosity on the pressure.
- Oscillatory behavior of the two motions and the influence of Weissenberg number and the pressure-viscosity coefficient on fluid velocity was graphically underlined and discussed.
- Similar solutions corresponding to the same problem of ordinary IMF and of INF with power-law dependence of viscosity on the pressure have been obtained as limiting cases of the present results using suitable asymptotic approximations of Bessel functions.
- Steady solutions for the simple Couette flow of IMF with power-law dependence of viscosity on the pressure have been also determined and the convergence of $u_{cp}(y, t)$, $\tau_{cp}(y, t)$ and $\sigma_{cp}(y, t)$ to these solutions was graphically proved when $\omega \rightarrow 0$.
- The shear stress τ_{Cp} corresponding to this motion is constant on the entire flow domain although the velocity $u_{Cp}(y)$ and normal stress $\sigma_{Cp}(y)$ are functions of the spatial variable y .

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